# Paraxial Approximation in CSR Modeling Using the Discontinuous Galerkin Method 

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## Introduction and Outline

- Well-established paraxial approximation in CSR has been previously modeled with a finite difference (FD) method.
- Novel approach in applying a discontinuous Galerkin (DG) method to the same equations.
- Starting point: nonhomogeneous Schrödinger type equations which arise from a paraxial approximation to Maxwell's equations.
- Include brief overview of DG and its implementation into our algorithm.
- Apply DG on a 2 D transverse $(x, y)$ grid and evolve the equations along the arclength $s$.
- Estimate the errors of our results and compute the longitudinal impedance.
- Discuss CPU vs GPU performance.
- Outline possible future work and new applications for DG.


## Mathematical Problem

## - Domain of problem

Consider rectangular domain with $(x, y) \in \Omega=$ $[-a, a] \times[-b, b]$ and $s \in[0, L]$. Additional parameters satisfy: $k \in \mathbb{R}$ and $\rho>0$.

- Paraxial PDEs for $\mathbf{E}^{r}(x, y, s ; k)$ :
$\partial_{s} E_{x}^{r}=\frac{i}{2 k} \nabla_{\perp}^{2} E_{x}^{r}+\frac{i k x}{\rho} E_{x}^{r}+\frac{i k x}{\rho} E_{x}^{b}(x, y)$ $\partial_{s} E_{y}^{r}=\frac{i}{2 k} \nabla_{\perp}^{2} E_{y}^{r}+\frac{i k x}{\rho} E_{y}^{r}+\frac{i k x}{\rho} E_{y}^{b}(x, y)$
$E_{s}^{r}=\frac{i}{k}\left(\partial_{x} E_{x}^{r}+\partial_{y} E_{y}^{r}\right)$
- Known beam component of field $\mathbf{E}^{b}$ :
$E_{x}^{b}=C \frac{x}{x^{2}+y^{2}}, \quad E_{y}^{b}=C \frac{y}{x^{2}+y^{2}} \quad$ (2)
- Boundary conditions for $E_{x, y}^{r}(x, y, s ; k)$ :

$$
\begin{array}{rlll}
\partial_{x} E_{x}^{r}=\partial_{y} E_{y}^{b}, & \text { on } & x= \pm a \\
E_{x}^{r}=-E_{x}^{b}, & \text { on } & y= \pm b, \\
E_{y}^{r}=-E_{y,}^{b}, & \text { on } & x= \pm a \\
\partial_{y} E_{y}^{r}=\partial_{x} E_{x}^{b}, & \text { on } & y= \pm b .
\end{array}
$$

- Initial conditions for $E_{x, y}^{r}(x, y, s ; k)$ :
$\nabla_{\perp}^{2} E_{x}^{r}=0, \quad \nabla_{\perp}^{2} E_{y}^{r}=0, \quad$ at $s=0 \quad$ (5)


## Physical Problem

- Beam Setup

Consider a line charge moving at $v \approx c$, on a circular arc of radius $\rho$ and length $L$, with perfectly conducting rectangular vacuum chamber.

- Beam coordinate system.

Adopt special case with line charge reduced to a single point. Maxwell's equations written in beam coordinates $(x, y, s)$ where the arc is in the $(x, s)$ plane, $s$ is the distance along the arc, and $(x, y)$ are perpendicular to arc.

- Electric field transformation.

Relate the electric field $\mathcal{E}(x, y, s, t)$ to frequency domain field $\mathbf{E}(x, y, s ; k)$ by Fourier-type transformation:

$$
\mathcal{E}(x, y, s, t) \propto \int_{-\infty}^{\infty} d k \mathbf{E}(x, y, s ; k) e^{i k(s-t)}
$$

- Initial condition of the electric field.

Assume fields reached steady-state from infinite straight prior to entering bend. Decompose electric field $\mathbf{E}$ into two components: radiation and beam field denoted by $\mathbf{E}^{r}$ and $\mathbf{E}^{b}$ respectively. $\mathbf{E}^{b}$ reduces the effect of the singularity.

## DG Overview

- DG shares similarities with the finite element and finite volume methods.
- Rescale to dimensionless variables:
$x \rightarrow a x, y \rightarrow a y, s \rightarrow 2 k a^{2} s, E_{x, y}^{r} \rightarrow C u / a$
- Equations (1a) and (1b) become:
$-i \partial_{s} u=\partial_{x} q_{x}+\partial_{y} q_{y}+F$
$q_{x}=\partial_{x} u, \quad q_{y}=\partial_{y} u$
- $\operatorname{Split} \Omega$ into K elements, select single element $D$.
- Local solution $u \in P^{N}(D)$.
- Multiply (6) by test functions $v \in P^{N}(D)$, integrate by parts over $D$, adjust boundary terms for fluxes $\left(u^{*}, q_{x}^{*}, q_{y}^{*}\right)$, and integrate by parts again:
$-i \int_{D} d A\left(v \partial_{s} u\right)=\int_{D} d A v\left(\partial_{x} q_{x}+\partial_{y} q_{y}+F\right)$ $-\int_{\partial D} d L v\left[n_{x}\left(q_{x}-q_{x}^{*}\right)+n_{y}\left(q_{y}-q_{y}^{*}\right)\right] \quad$ (7a) $\int_{D} d A\left(v v_{x, y}\right)=\int_{D} d A v\left(\partial_{x, y}, v^{2}\right.$
$-\int_{\partial D} d L n_{x, y}\left(u-u^{*}\right)$
- Expand local solution in nodal Lagrange basis:
$u(x, y)=\sum_{i=1}^{N_{n}} w_{f}(x, v, v) v(x, y)=\ell_{f}(x, y)$
- Vectors for nodal values $\mathbf{u}=\left(u_{1}, u_{2}, \ldots, u_{N_{p}}\right)^{T}$ with $N_{p}=(N+1)(N+2) / 2$.
- Similarly for $q_{x, y}, F, \ell$, then (7a)-(7b) become:

$$
\begin{aligned}
&-i \mathcal{M} \frac{d \mathbf{u}}{d s}=\mathcal{S}_{x} \mathbf{q}_{x}+\mathcal{S}_{y} \mathbf{q}_{y}+\mathcal{M} \mathbf{F} \\
&-\int_{\partial D} d L n_{x}\left(\mathbf{q}_{x}-\mathbf{q}_{x}^{*}\right) \boldsymbol{\ell} \\
&-\int_{\partial D} d L n_{y}\left(\mathbf{q}_{y}-\mathbf{q}_{y}^{*}\right) \boldsymbol{\ell} \\
& \mathcal{M} \mathbf{q}_{x}=\mathcal{S}_{x} \mathbf{u}-\int_{\partial D} d L n_{x}\left(\mathbf{u}-\mathbf{u}^{*}\right) \boldsymbol{\ell} \\
& \mathcal{M} \mathbf{q}_{y}=\mathcal{S}_{y} \mathbf{u}-\int_{\partial D} d L n_{x}(\mathbf{u}) \\
&\left.\mathbf{u}-\mathbf{u}^{*}\right) \boldsymbol{\ell}
\end{aligned}
$$

- Mass and stiffness matrices:
$\mathcal{M}_{i j}=\int_{D} d A \ell_{i} \ell_{j}, \quad\left(\mathcal{S}_{x, y}\right)_{i j}=\int_{D} d A\left(\partial_{x, y} \ell_{i}\right) \ell_{j}$
- Numerical fluxes depend on adjacent elements:

$$
q_{x, y}^{*}=\left\{\left\{q_{x, y}\right\}\right\}-\tau[u]_{x, y}, \quad u^{*}=\{\{u\}\}
$$

- Full details found in Nodal Discontinuous Galerkin Methods, (New York: Springer, 2008) by J. Hesthaven and T. Warburton.


## DG Algorithm

Step 1: Build Elements and Matrices

- Partition $\Omega$ into $K=2 N_{x}^{\text {res }} N_{y}^{\text {res }}$ triangles and space nodes optimally for matrix conditioning.


Figure 1: Mesh of $N_{x}^{\text {res }}=6, N_{y}^{\text {res }}=2, N=4$.

- Build collocation derivative matrices: $\mathcal{D}_{x}$ $\mathcal{M}^{-1} \mathcal{S}_{x}$ and $\mathcal{D}_{y}=\mathcal{M}^{-1} \mathcal{S}_{y}$.
Step 2: Compute Initial Conditions
- Use sparse DG Poisson solver on (5) with (3), (4) to obtain initial $E_{x, y}^{r}$.
- Generate initial $E_{s}^{r}$ with derivative matrices:

$$
E_{s}^{r}=\frac{i}{k}\left(\mathcal{D}_{x} E_{x}^{r}+\mathcal{D}_{y} E_{y}^{r}\right)
$$ (10)

DG Algorithm Cont.


Figure 2: $E_{x}^{r}$ initial state prior to entering bend
Step 3: Evolve the Fields

- Estimate step size for evolution by
$\Delta s=C_{s} \cdot k \cdot r_{\text {min }}^{2}$
$r_{\text {min }}$ is the minimum distance between all nodes, $C_{s}$ is CFL-like constant of $\mathcal{O}(1)$. Note: $r_{\text {min }} \propto$ $1 /\left(K N^{2}\right)$
- Compute $\mathbf{q}_{x, y}$ with (8b)-(8c) and insert into (8a) for right-hand-side of $d \mathbf{u} / d s$.
- Use 4th order explicit Runge-Kutta to evolve
- At each step, compute $E_{s}^{r}$ with (10).

${ }^{y(\text { mim })}$ Figure 3: Real (top) ${ }^{x(\text { man })}$ and imaginary (bottom) parts of $E_{x}^{r}$ after bend for $a=30 \mathrm{~mm}, b=10 \mathrm{~mm}$, $L=200 \mathrm{~mm}, \rho=1 \mathrm{~m}$, and $k=8 \mathrm{~mm}^{-1}$
Step 4: Compute Impedance
- Evaluate impedance $Z$ in two parts:

$$
\begin{aligned}
Z & =Z_{b}+Z_{s} \\
Z_{b} & =-\frac{Z_{0}}{2 \pi C} \int_{0}^{L} d s E_{s}(0,0, s ; k) \\
Z_{s} & =-\frac{Z_{0}}{2 \pi C} \int_{L}^{\infty} d s E_{s}(0,0, s ; k)
\end{aligned}
$$

- For details on the evaluation of $Z$, see D. Zhou's paper: Jpn. J. Appl. Phys. 51016401 (2012).

Numerical Results: DG

DG $E_{x}^{r}$ Error and Computation Time | $\mathbf{N} \backslash \mathbf{K}$ | $\mathbf{1 5 0}$ | $\mathbf{6 0 0}$ | $\mathbf{1 3 5 0}$ | $\mathbf{2 4 0 0}$ |
| :---: | ---: | ---: | ---: | ---: |
|  | $8.107 \mathrm{e}-1$ | $3.915 \mathrm{e}-1$ | $7.471 \mathrm{e}-2$ | $2.453 \mathrm{e}-2$ |

 \begin{tabular}{r|r|r|r|}
\hline 9 s \& 28 s \& 49 s \& 81 s <br>
122 \& 486 \& 1093 \& 1943 <br>
\hline

 $1.265 \mathrm{e}-14.897 \mathrm{e}-3 \quad 9.344 \mathrm{e}-4 \quad 3.590 \mathrm{e}-4$ 8.017e-2 $3.427 \mathrm{e}-39.462 \mathrm{e}-44.342 \mathrm{e}-4$ 

29 s \& 88 s \& 202 s \& 392 s <br>
539 \& 2156 \& 4850 \& 8622

 $\begin{array}{rrrrr}539 & 2156 & 4850 & 8622 \\ 1.122 e-2 & 5.177 e-4 & 1.407 e-4 & 5.483 e-5\end{array}$ $6 \quad 6.974 \mathrm{e}-36.187 \mathrm{e}-41.932 \mathrm{e}-48.045 \mathrm{e}-5$ 

83 s \& 283 s \& 677 s \& 1319 s <br>
1691 \& 6764 \& 1518 \& 270

 

1691 \& 6764 \& 15218 \& 27054 <br>
\hline

 

$1.569 e-3$ \& $1.672 e-4$ \& $5.612 e-5$ \& $\mathrm{~N} \backslash \mathrm{~A}^{*}$ <br>
$1.493-3$ \& $2.09 \mathrm{~B}^{2}-4$ \& $7.47 \mathrm{e}-5$ \& $\mathrm{~N} \backslash \mathrm{~A}^{*}$

 $\begin{array}{rrrr}1.493 \mathrm{e}-3 & 2.098 \mathrm{e}-4 & 7.473 \mathrm{e}-5 & \mathrm{~N}^{2} \backslash \mathrm{~A}^{*} \\ 208 \mathrm{~s} & 723 \mathrm{~s} & 1867 \mathrm{~s} & 3630 \mathrm{~s}\end{array}$ 

208 s \& 723 s \& 1867 s \& 3630 s <br>
4174 \& 16693 \& 37559 \& 66771 <br>
\hline
\end{tabular}

