

Locking Phenomena in the Material Point Method

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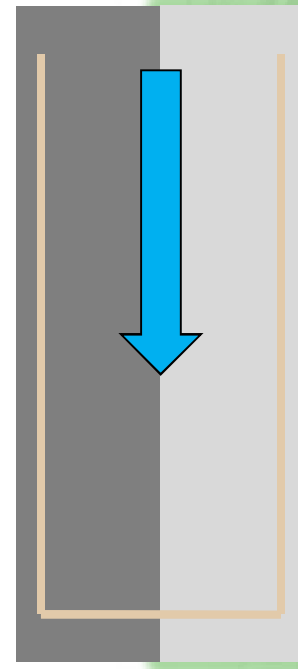
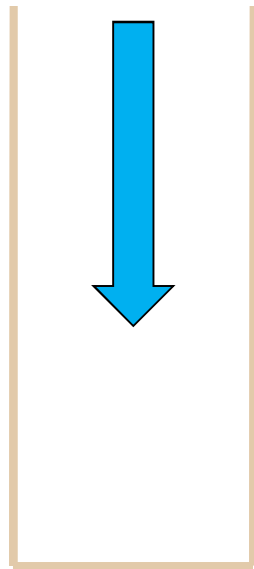
Overview

- **Introduction**
- **Sources of Locking**
 - Low order shape functions
 - Convection of a stressed body
- **Problem Resolution Approach**
 - Volumetric Locking
 - Shear Locking
- **Summary and Conclusions**

Introduction


- Last year's workshop:
 - Modeling fluid as nearly incompressible viscous material

Burst of water into a glass



The Locking Problem

Volumetric locking
intrinsic
to the MPM

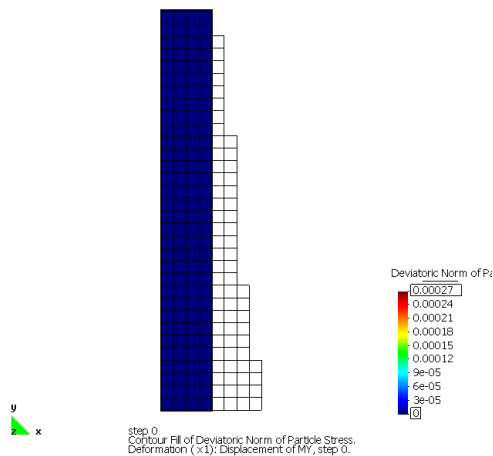


- **Proposed solution for locking**

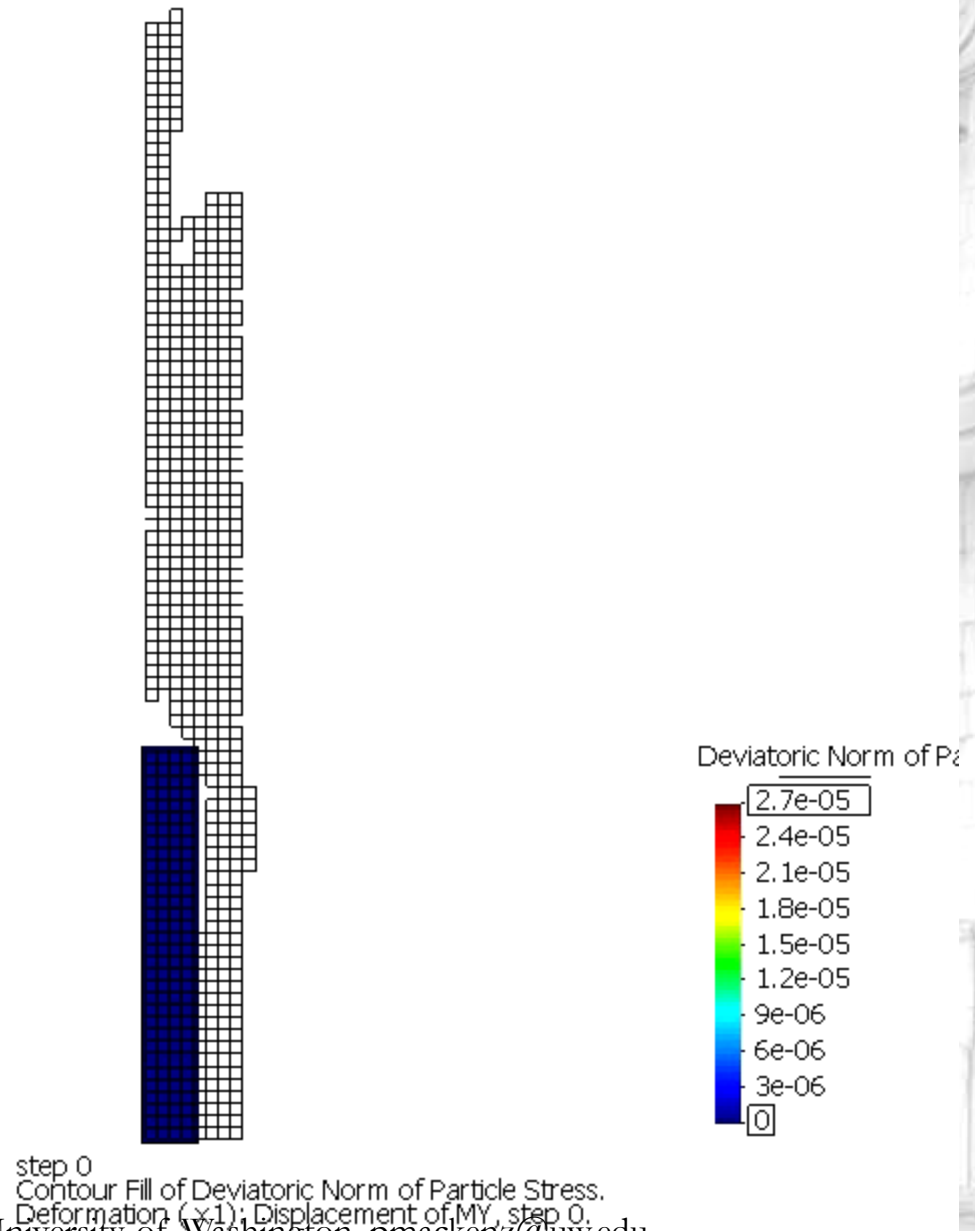
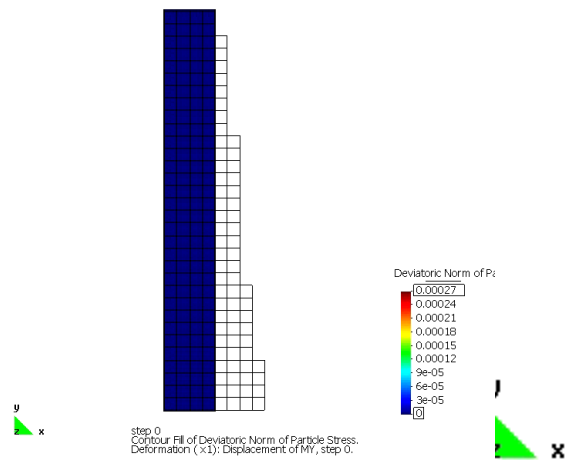
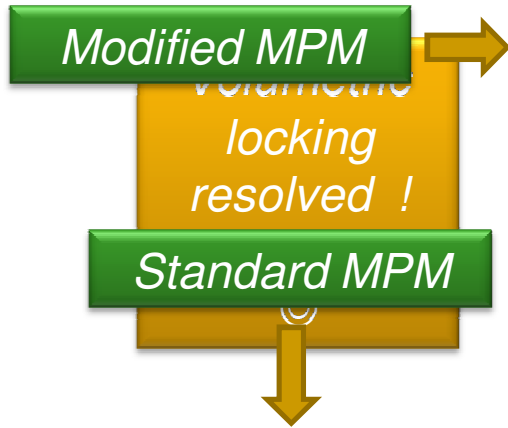
- Kinematic constraints on the background grid relaxed by smoothed volume change

$$\Rightarrow \bar{\theta} = \frac{\sum_{p \in CV} \text{tr } \boldsymbol{\varepsilon}_p m_p / \rho_p}{\sum_{p \in CV} m_p / \rho_p}$$

$$\Rightarrow p := \bar{p}_{CV} = \rho \frac{\partial \bar{U}(\bar{\theta})}{\partial \bar{\theta}}$$



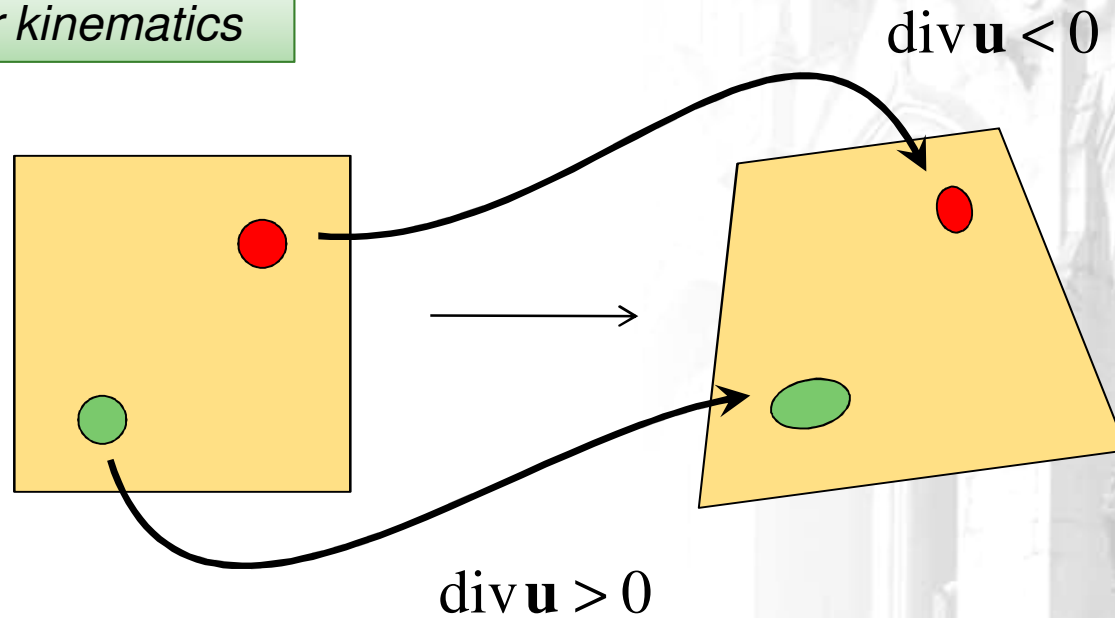
Anti-Locking Strategy



Sources of Locking

- Shape change \gg “Volumetric Locking”

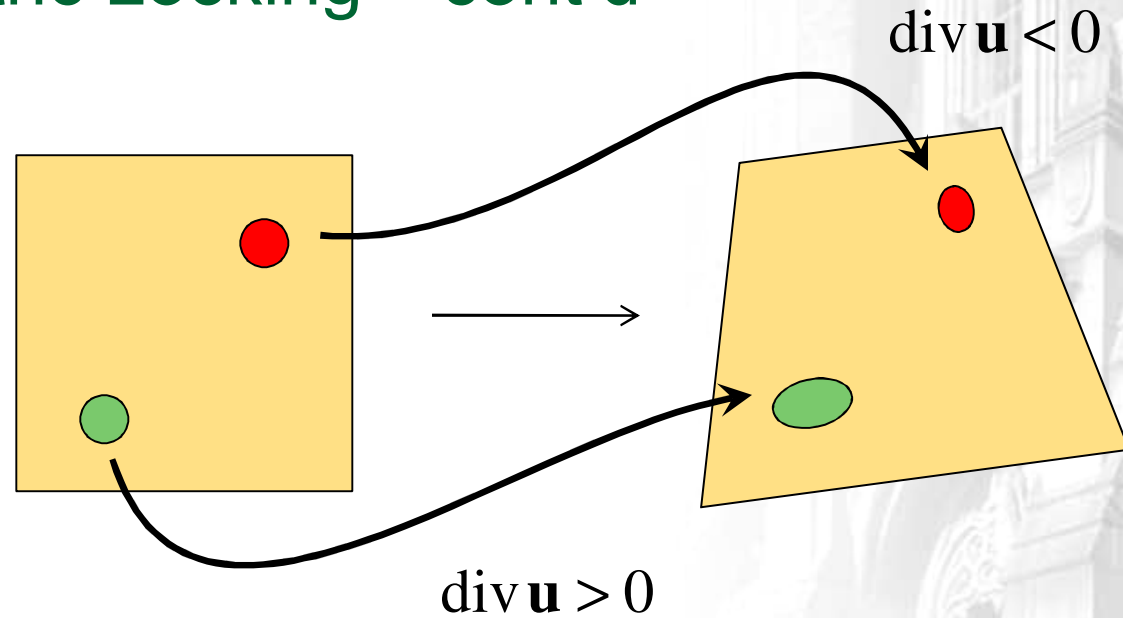
Low-order kinematics



Excess energy

$$E = \int_{\Omega} \frac{1}{2} k (\text{div } \mathbf{u})^2 d\Omega > 0$$

Volumetric Locking – cont'd



$$\int_{CV} (\bar{\theta} - \text{div } \mathbf{u}) w \, dm = 0 \quad \Rightarrow \quad \bar{\theta} = \frac{\int_{CV} \text{div } \mathbf{u} \, dm}{\int_{CV} dm}$$

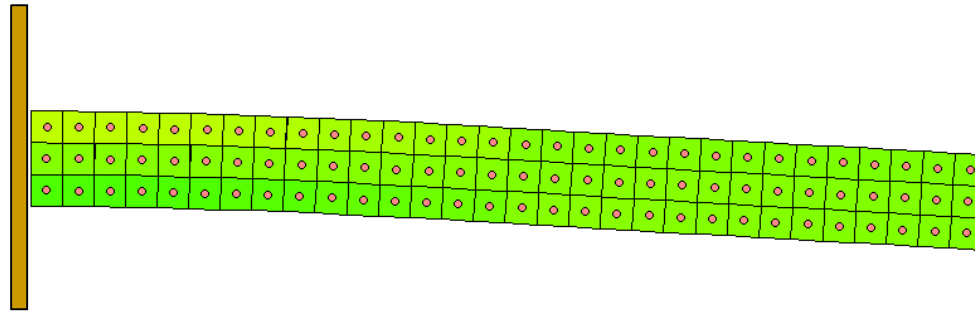
$$\Rightarrow p = \rho \bar{k} \bar{\theta}$$

$$E = \int_{CV} \frac{1}{2} \bar{p} \text{div } \mathbf{u} \, dm = \frac{1}{2} \bar{k} \bar{\theta}^2 m_{\Omega} \rightarrow 0$$

Sources of Locking

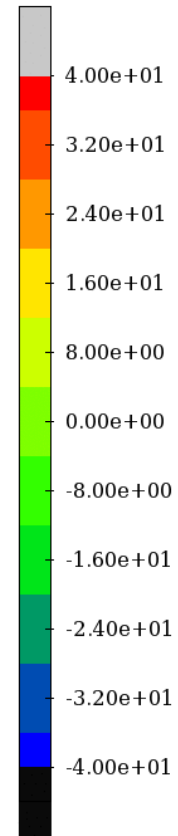
■ Vibrating beam:

- initial velocity proportional to 1st mode shape (stress-free)



Period MPM = 0.92 T (~7% error)

Sigma XX

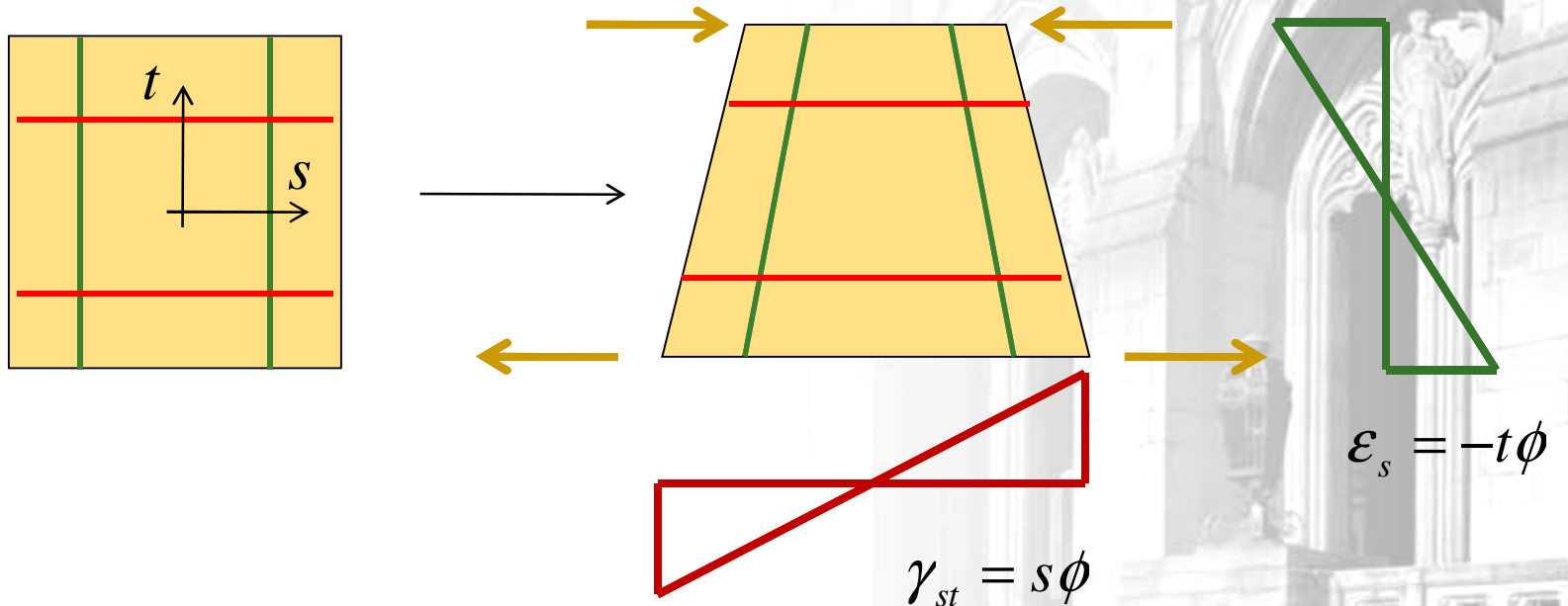


Time: 0.5000 sec

Sources of Locking

- Bending deformation \gg “Shear Locking”

Low-order kinematics

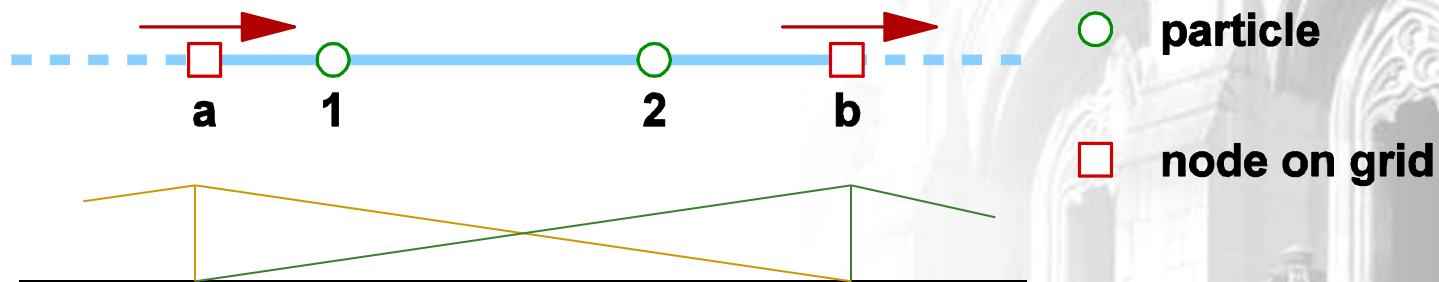


Excess energy

$$E^h = \frac{1.5 + \nu}{1 + \nu} E_{bending}$$

Sources of Locking

- Convection of a stressed body in quasi-static equilibrium
 - Known as “cell crossing error”

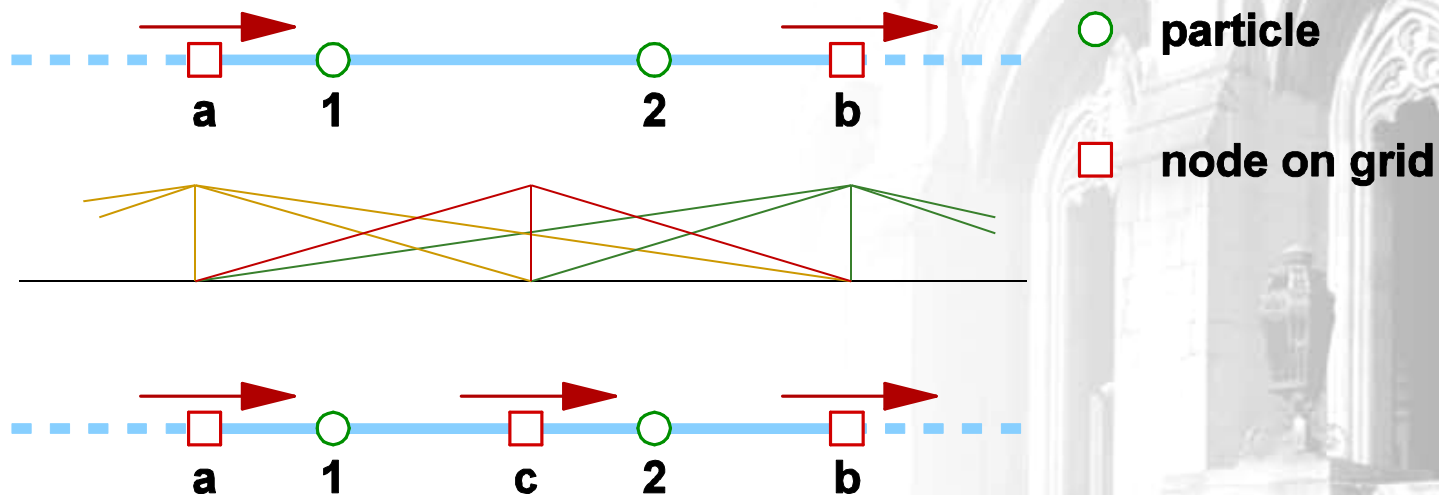


$$f_a = \frac{1}{h} (\sigma_1 m_1 + \sigma_2 m_2)$$

$$f_b = -\frac{1}{h} (\sigma_1 m_1 + \sigma_2 m_2)$$

Sources of Locking

- Convection of a stressed body in quasi-static equilibrium
 - Known as “cell crossing error”

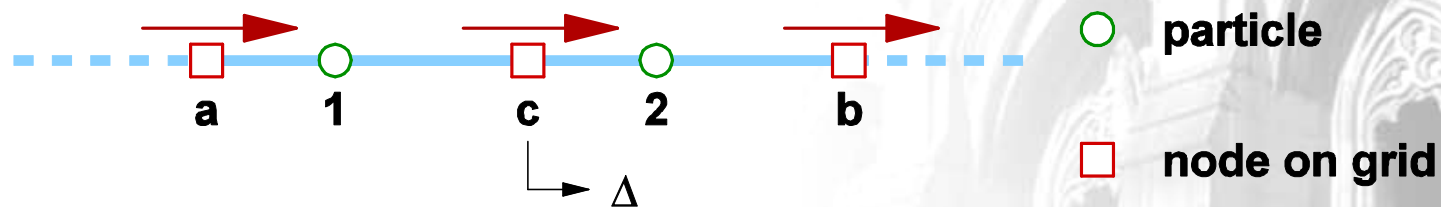


The black sheep

$$f_c = \frac{2}{h} (-\bar{\sigma}_1 m_1 + \bar{\sigma}_2 m_2) \neq 0$$

Sources of Locking

- Convection of a stressed body in quasi-static equilibrium



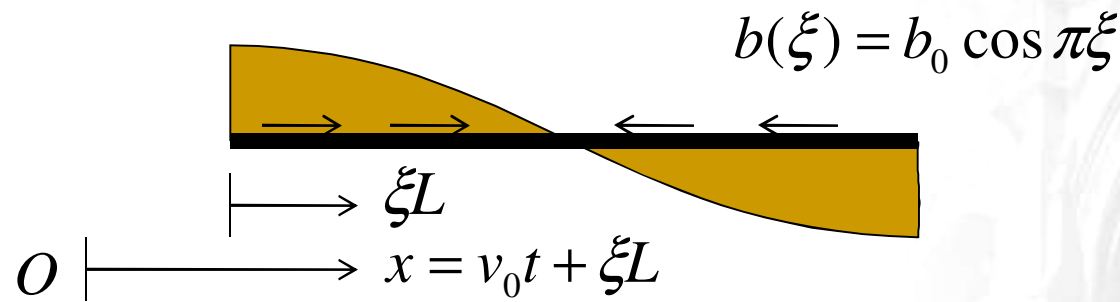
$$f_c = \frac{2}{h} (-\bar{\sigma}_1 m_1 + \bar{\sigma}_2 m_2) \neq 0 \quad \Rightarrow \text{find } \Delta \text{ such that } f_c = 0$$

$$\bar{\sigma}_1 \rightarrow \frac{2m_1 + m_2}{m_1 + m_2} \bar{\sigma}_1 - \frac{m_2}{m_1 + m_2} \bar{\sigma}_2$$

$$\bar{\sigma}_2 \rightarrow -\frac{m_1}{m_1 + m_2} \bar{\sigma}_1 + \frac{m_1 + 2m_2}{m_1 + m_2} \bar{\sigma}_2$$

Problem Resolution Approach

- Convection of a stressed body in quasi-static equilibrium



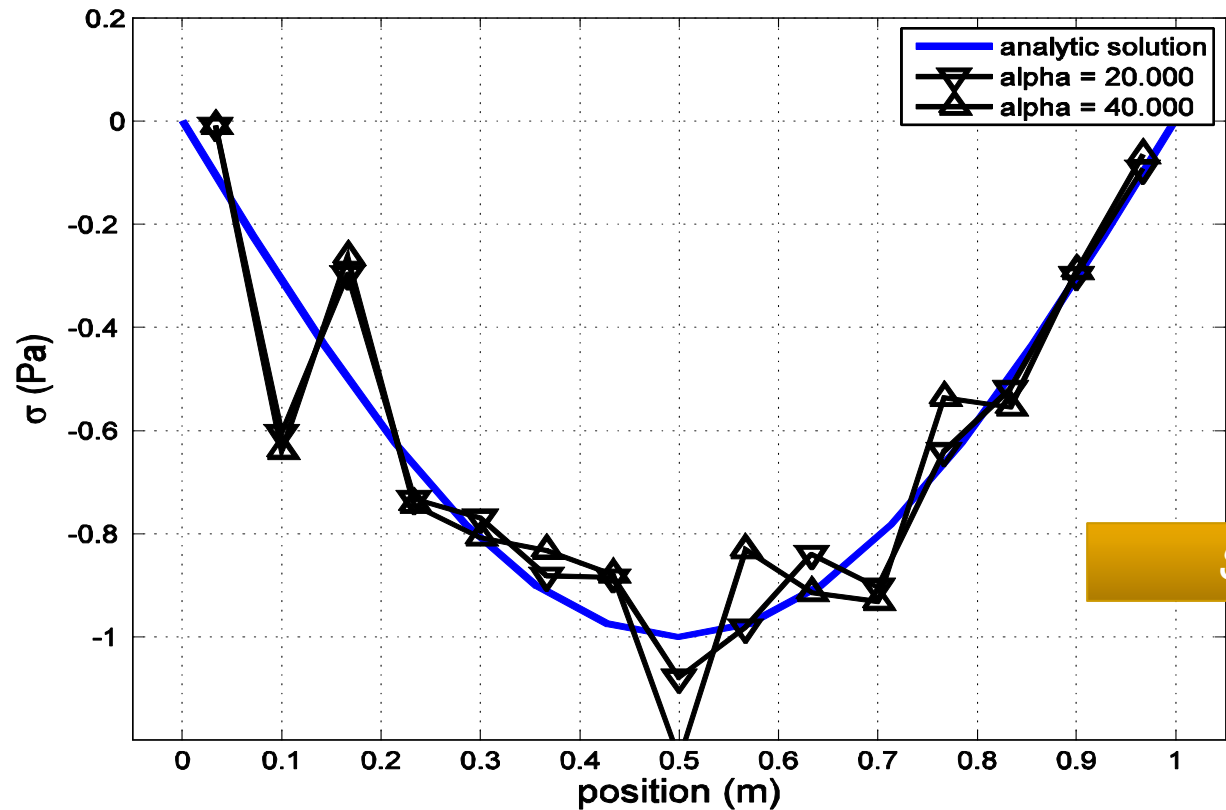
Analytic solution :

$$u(\xi) = v_0 t + \frac{b_0 L^2}{\pi^2 EA} (\cos \pi \xi - 1)$$

$$\sigma(\xi) = -\frac{b_0 L}{\pi A} \sin \pi \xi$$

Problem Resolution Approach

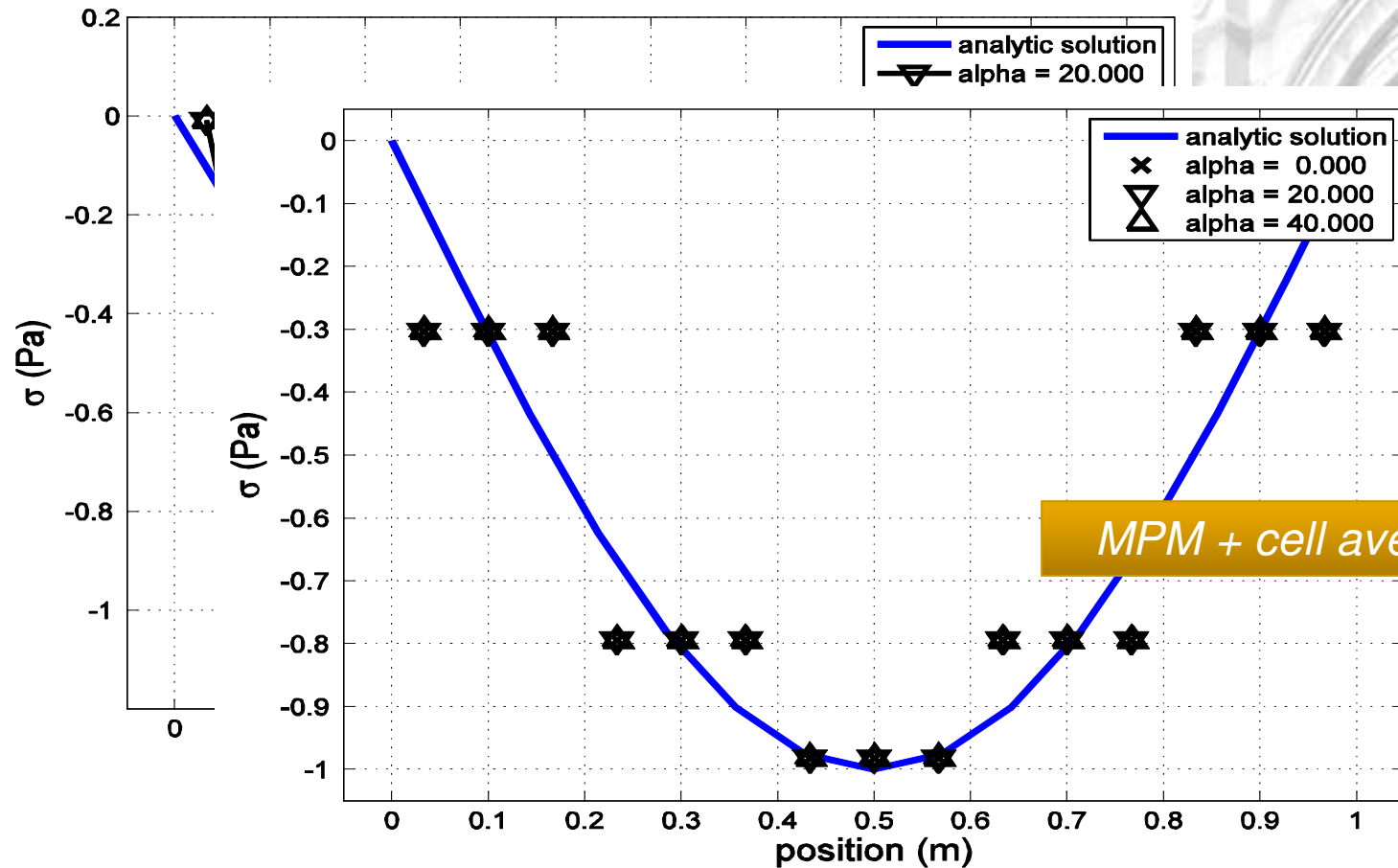
- Convection of αL in 1000 steps / L (5 cells/ L)



Standard MPM

Problem Resolution Approach

- Convection of αL in 1000 steps / L (5 cells/ L)



Problem Resolution Approach

- 2D/3D >> Filtering of strain/stress fields

$$\int_m \psi(\boldsymbol{\varepsilon}^h) dm - \int_m \bar{\mathbf{b}} \cdot \boldsymbol{\chi} dm - \int_{\partial V_\sigma} \bar{\mathbf{t}} \cdot \boldsymbol{\chi} dS + \int_m \bar{\boldsymbol{\sigma}}^h : (\boldsymbol{\varepsilon}(\mathbf{u}^h) - \boldsymbol{\varepsilon}^h) dm \rightarrow \text{stationary}$$

$$\{\bar{\boldsymbol{\sigma}}^h\} := \begin{Bmatrix} \bar{\sigma}_{ss} \\ \bar{\sigma}_{tt} \\ \bar{\sigma}_{st} \end{Bmatrix} \rightarrow \underbrace{\begin{bmatrix} 1 & 0 & 0 & t & 0 \\ 0 & 1 & 0 & 0 & s \\ 0 & 0 & 1 & 0 & 0 \end{bmatrix}}_{=:\mathbf{S}} \underbrace{\begin{Bmatrix} \beta_1 \\ \beta_2 \\ \beta_3 \\ \beta_4 \\ \beta_5 \end{Bmatrix}}_{=:\boldsymbol{\beta}} \quad \{\boldsymbol{\varepsilon}^h\} := \begin{Bmatrix} \boldsymbol{\varepsilon}_{ss} \\ \boldsymbol{\varepsilon}_{tt} \\ 2\boldsymbol{\varepsilon}_{st} \end{Bmatrix} \rightarrow [\mathbf{S}]\{\boldsymbol{\alpha}\}$$

Problem Resolution Approach

- 2D/3D >> Filtering of strain/stress fields

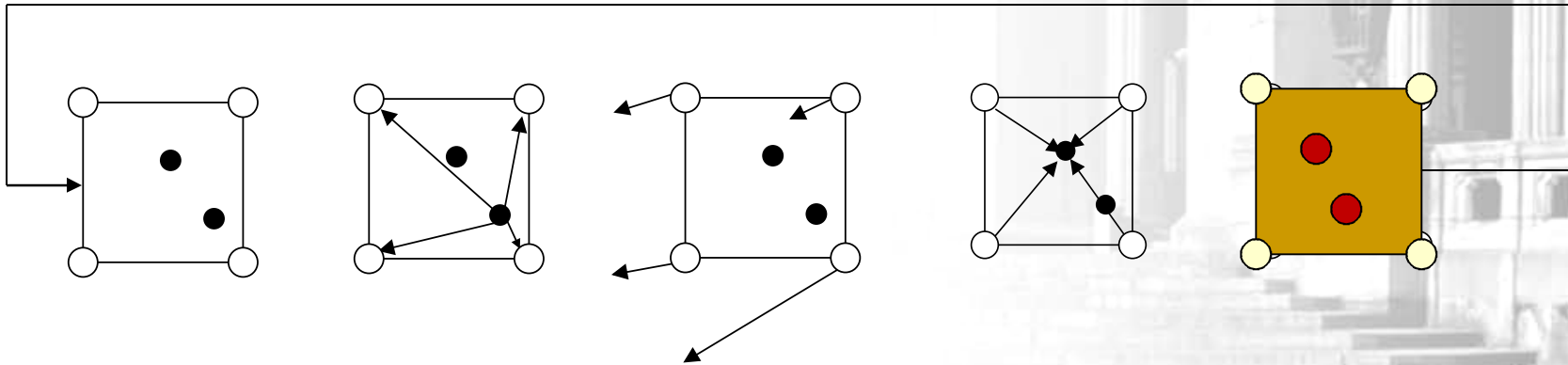
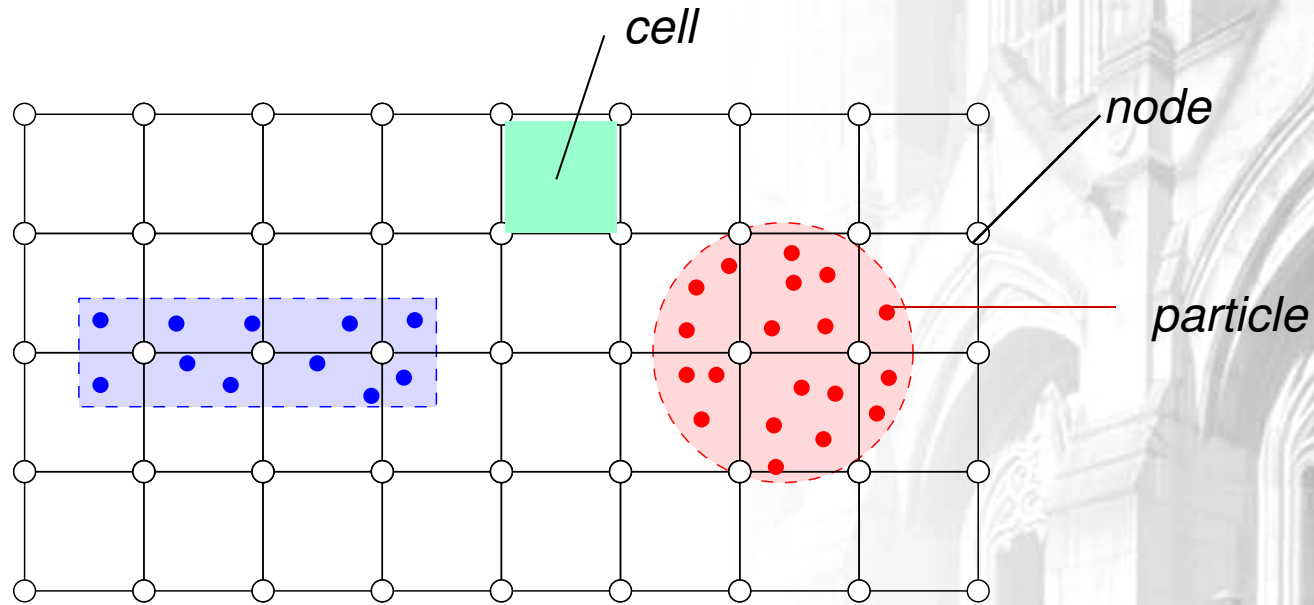
For each cell c

$$[\mathbf{H}_c] := \sum_{p \in c} [\mathbf{S}_p]^t [\mathbf{S}_p] m_p \quad \Rightarrow \quad \{\boldsymbol{\beta}_c\} = [\mathbf{H}_c]^{-1} \{\mathbf{R}_c\}$$
$$\{\mathbf{R}_c\} := \sum_{p \in c} [\mathbf{S}_p]^t \{\bar{\boldsymbol{\sigma}}_p\} m_p$$

For each particle p in cell c

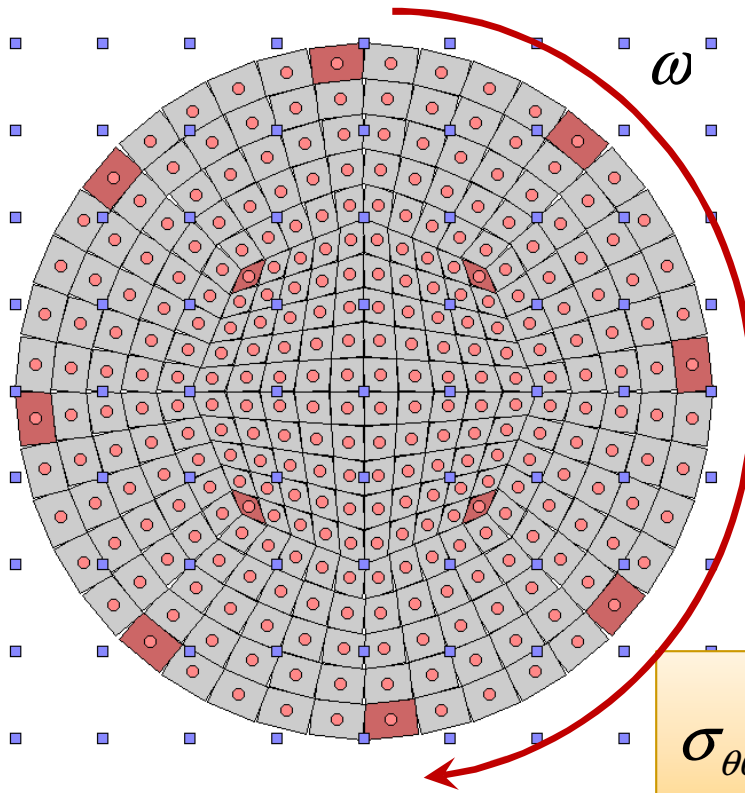
$$\{\bar{\boldsymbol{\sigma}}_p\} \rightarrow [\mathbf{S}_p] \{\boldsymbol{\beta}_c\} \quad \Rightarrow \quad \begin{array}{l} \text{elastic} \\ \text{plastic} \end{array} \quad \Rightarrow \quad \begin{array}{l} \{\boldsymbol{\varepsilon}_p\} = [\mathbf{C}]^{-1} \{\bar{\boldsymbol{\sigma}}_p\} \\ \{\boldsymbol{\varepsilon}_p\} \rightarrow [\mathbf{S}_p] \{\boldsymbol{\alpha}_c\} \end{array}$$

Adding Smoothing to the Basic Algorithm



The Ultimate Challenge

Spinning Disk



Velocity field at time 0.0000 sec

Initial conditions

$$u_r = 0$$

$$u_\theta = r\omega$$

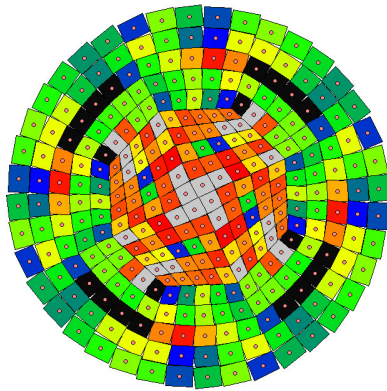
$$\sigma_{rr} = \frac{\rho\omega^2}{8}(3+\nu)(a^2 - r^2)$$

$$\sigma_{\theta\theta} = \frac{\rho\omega^2}{8}((3+\nu)a^2 - (1+3\nu)r^2)$$

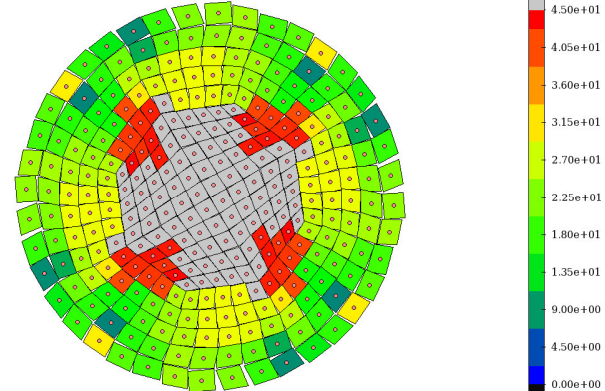
$$\sigma_{r\theta} = 0$$

The Ultimate Challenge: Spinning Disk $\sigma_{rr} = const.?$

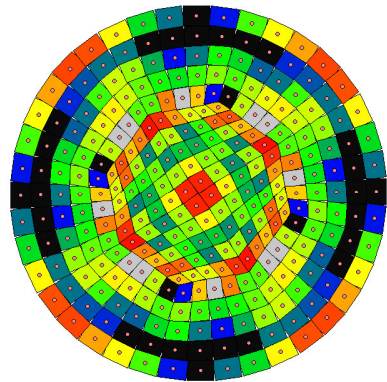
Standard MPM



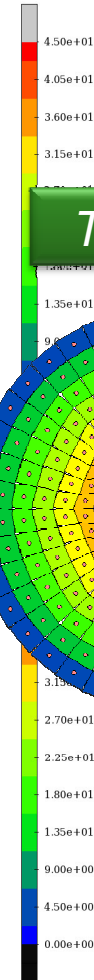
MPM+stress smoothing



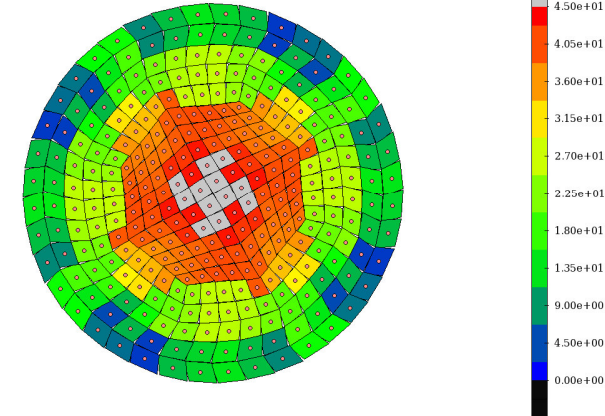
CPDI



Sigma RR



CPDI+stress smoothing

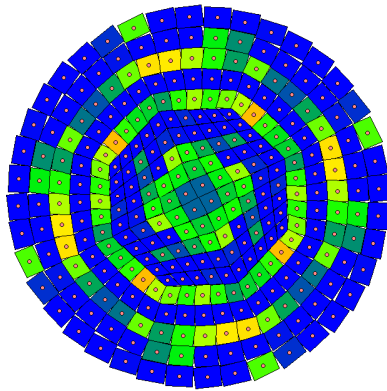


Time: 6.2000 sec

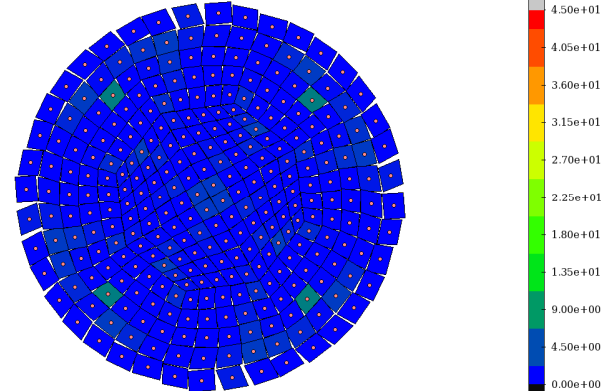
After almost one full revolution

The Ultimate Challenge: Spinning Disk $\sigma_{r\theta} = 0$?

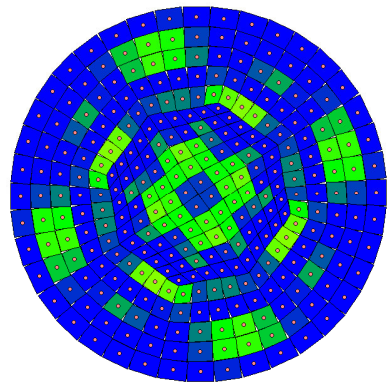
Standard MPM



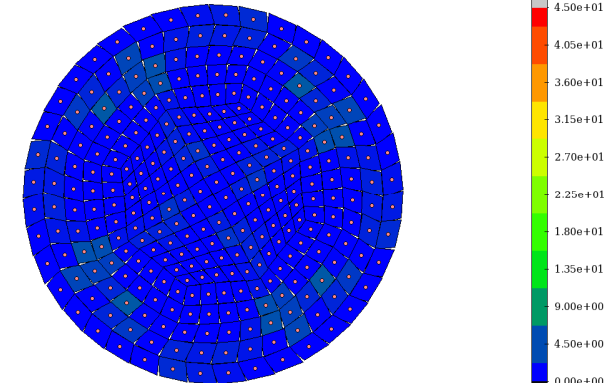
MPM+stress smoothing



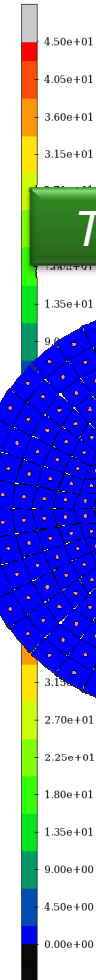
CPDI



CPDI+stress smoothing



Sigma RT



TARGET

Time: 6.2000 sec

After almost one full revolution

Summary & Conclusions

- We identified that, thanks to using identical shape functions, **MPM inherited locking from the FEM**.
- We interpret the “**cell crossing error**” as “**convection locking**”.
- We propose a cell-based **smoothing strategy that filters/removes locking stresses/strains** from the numerical solution.
- The proposed technique **improves solutions for both standard MPM and CPDI** but **does not completely eliminate the problem (yet)** .



Questions ?

August 9-10, 2010

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6th MPM Workshop @ U of New Mexico: Locking Phenomena in MPM

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