

Evaluation of a Smeared Crack Approach in MPM as a Computational Failure Method

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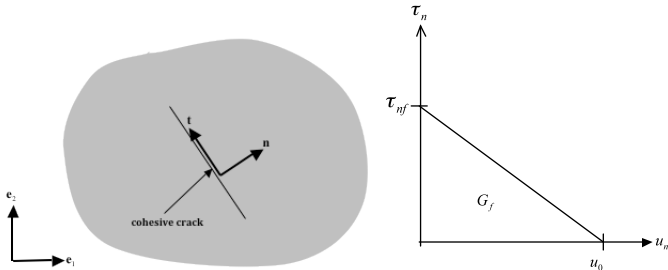
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Motivation and Objective

- Smearred crack MPM used to model opening of leads (cracks) in sea ice motion [Sulsky et al., 2007], [Peterson, 2008]
- Assess limitations of smearred crack MPM as a computational fracture method
- Implicit dynamics MPM utilized [Sulsky and Kaul, 2004]

Discrete Constitutive Models for Material Failure

Represents FPZ in quasi-brittle failure such as concrete by relating traction to the jump in the displacement discontinuity across a failure surface [Hillerborg et al., 1976], [Schreyer, 2007]



$$\{\mathbf{n}, \mathbf{t}\}$$

$$\boldsymbol{\tau} = \tau_n \mathbf{n} + \tau_t \mathbf{t}$$

$$[[\mathbf{u}]] = [[u_n]] \mathbf{n} + [[u_t]] \mathbf{t}$$

$$G_f$$

$$\tau_{nf}$$

$$u_0$$

failure surface basis

traction

displacement discontinuity

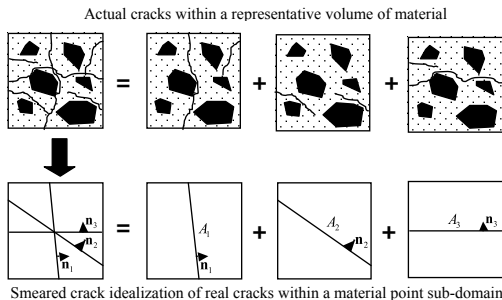
fracture energy

ultimate tensile strength

critical crack opening

Smearred Crack Representation of Failure

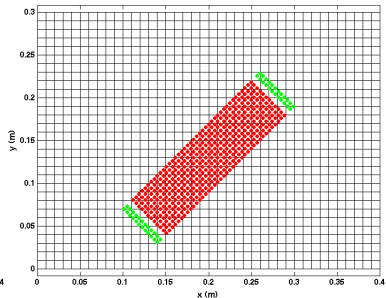
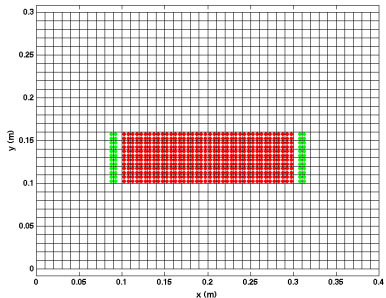
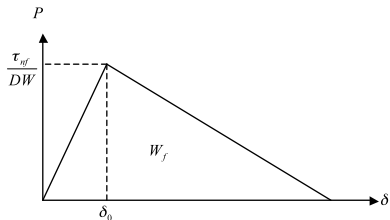
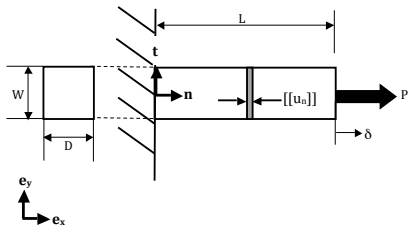
Smearred crack FEM: [Rots, 1988], [de Borst and Nauta, 1985], [Bazant and Oh, 1983]



$$\underbrace{\boldsymbol{\varepsilon}}_{\text{total strain}} = \underbrace{\boldsymbol{\varepsilon}^e}_{\text{elastic strain}} + \underbrace{\boldsymbol{\varepsilon}^{dc}}_{\text{de-cohesive strain}}$$

$$\boldsymbol{\varepsilon}^{dc} = \sum_i \boldsymbol{\varepsilon}_i^{dc}, \quad \boldsymbol{\varepsilon}_i^{dc} = \frac{1}{L_c} ([[\mathbf{u}]]_i \otimes \mathbf{n}_i)^S, \quad L_c \text{ characteristic length}$$

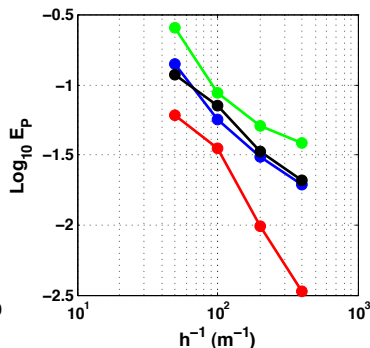
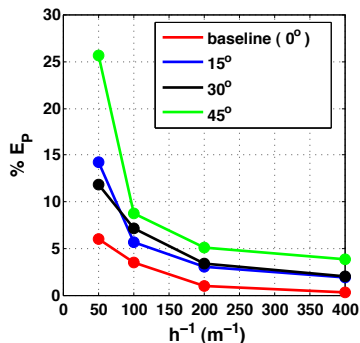
Case Study Problem: Elastic De-cohesive Tensile Bar



Preliminary Study:

Grid Orientation Bias for Elastic Tensile Bar

Rate of convergence affected for different $\alpha = \cos^{-1}(\mathbf{n} \cdot \mathbf{e}_x)$



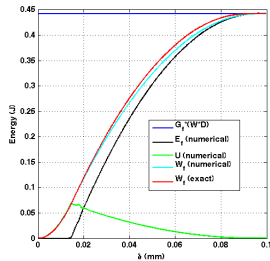
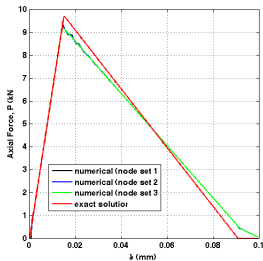
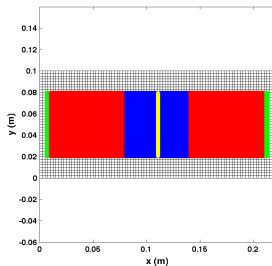
$$E_P = \frac{(P_{mpm} - P_{analytical})}{P_{analytical}} h$$

axial load error

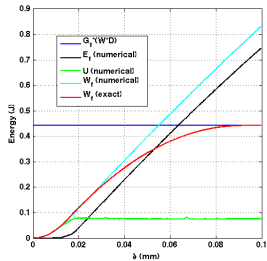
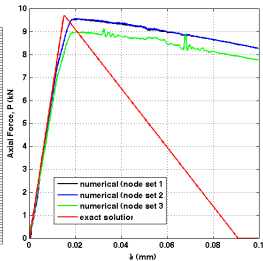
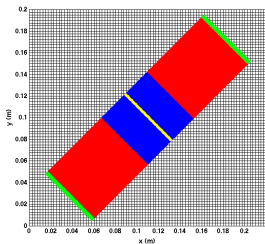
square grid cell side length

Grid Orientation Bias: Stiffening Effect

$\alpha = 0^\circ$

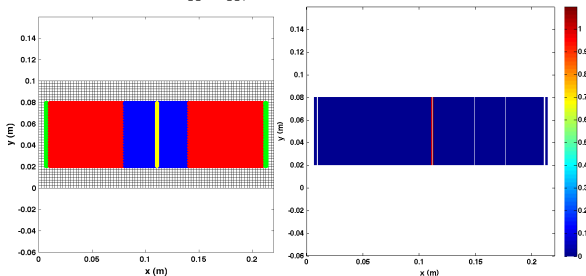


$\alpha = 45^\circ$

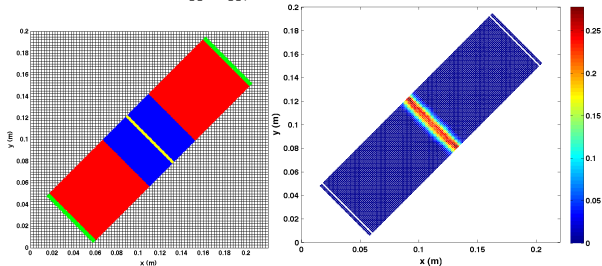


Grid Orientation Bias: Failure Pattern Spreading

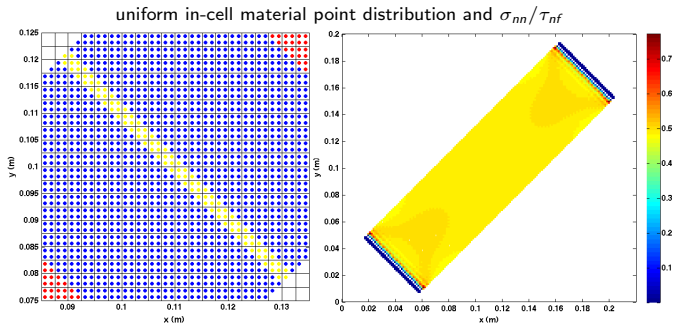
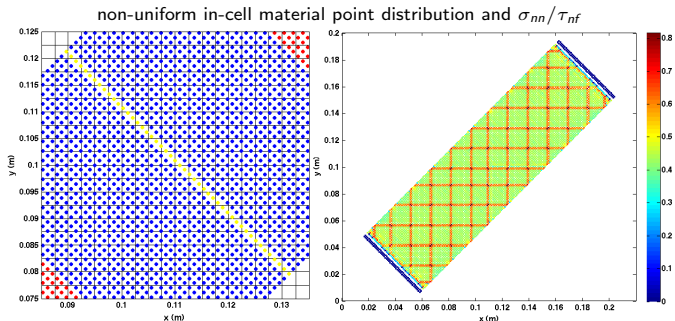
$[[u_n]]/u_0$ for $\alpha = 0^\circ$



$[[u_n]]/u_0$ for $\alpha = 45^\circ$

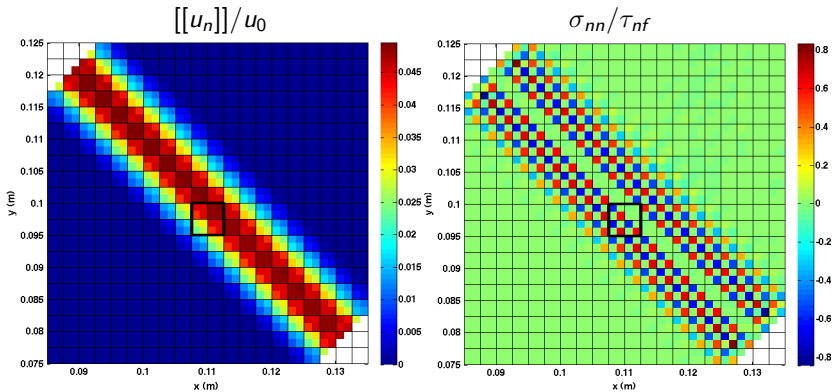


In-cell Material Point Distribution Effect on Stress Field



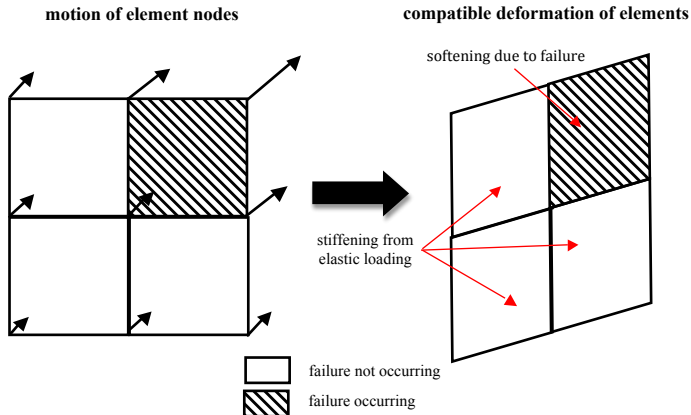
Investigation of failure zone

- Unphysical build-up of stress in failure region and spreading of failure zone



Compatibility

- Stress build-up \rightarrow stiffening
- Stress build-up in smeared crack MPM caused by compatibility of deformation imposed by the grid
- Stress build-up \longleftrightarrow spreading of failure zone
- "Stress locking" in smeared crack FEM [Rots, 1988]



Conclusions & Future Work

- Smearred crack MPM suffers from grid orientation bias
 - A stiffening and spreading of failure pattern occurs when failure surface and grid cell lines are not aligned
- Limited use of smearred crack MPM is recommended
- Embedded discontinuity [Oliver, 1996], [Oliver et al., 2003] MPM unsuccessful
- Future approaches for representing failure in MPM



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